Int. J. Solids Structures. 1978. Vol. 14. pp. 329–330. Pergamon Press. Printed in Great Britain

ERRATA

AYBAR ERTEPINAR, Large amplitude radial oscillations of layered thick-walled cylindrical shells. *Int. J. Solids Structures* **13**, 717–723 (1977).

1. The expression for S_i in eqn (9) should be corrected as

$$S_i = \frac{R_{i+1}^2}{R_1^2} - 1$$

2. Equations (16) should be corrected as

$$\int_1^\eta \eta\bar{p}\,\mathrm{d}\eta = \begin{cases} (p_{in}^0/\rho_0 R_1^2)\,\dfrac{\eta^{2(1-\alpha)}-1}{(1-\alpha)} & \text{for } \alpha \neq 1, \\ (p_{in}^0/\rho_0 R_1^2)\ln(\eta)^2 & \text{for } \alpha = 1, \end{cases}$$

$$\int_1^\eta \eta f_1(w)\,\mathrm{d}\eta = \frac{\phi_1}{2\rho_0 R_1^2}(1-\eta^2)\ln\frac{(\eta^2+S_1)}{\eta^2(S_1+1)}, \tag{16}$$

$$\int_1^\eta \eta f_2(w)\,\mathrm{d}\eta = \frac{\phi_2}{2\rho_0 R_1^2}(1-\eta^2)\ln\frac{(1+S_1)(\eta^2+S_2)}{(1+S_2)(\eta^2+S_1)}.$$

3. Equation (25) should be corrected as

$$H = \sqrt{(A^2-b^2)} - A - a^2(1+S_1)\frac{A}{\sqrt{(A^2-b^2)}} + \frac{(1+2P)a^2+b^2-1}{\sqrt{(1-b^2)}} + a^2(S_1-2P)+1$$
$$C\left[\frac{B^2-b^2-a^2B(S_2+1)}{\sqrt{(B^2-b^2)}} + \frac{a^2(S_1+1)A - A^2 + b^2}{\sqrt{(A^2-b^2)}}\right], \tag{25}$$

Viggo Tvergaard, Buckling of elastic–plastic oval cylindrical shells under axial compression. *Int. J. Solids Structures* **12**, 683–691 (1976).

The numerical values of bifurcation stresses in Fig. 2 are erroneous, and should be replaced by:

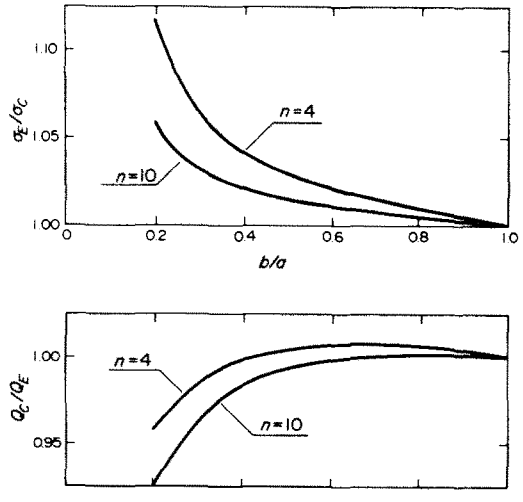

Fig. 2. Critical stress and corresponding axial wave length in elliptical cylinders with aspect ratio b/a. ($R_b/h = 200$, $\sigma_C/\sigma_y = 1.034$, $\sigma_y/E = 0.0025$, $\nu = 0.3$).

The 1–2% corrections of bifurcation stresses result in small changes of the post-bifurcation expansion, so that Table 1 should be replaced by:

Table 1. Constants in asymptotic post-bifurcation expansion for various elliptical cylinders made of material with $\nu = 0.3$

b/a	R_b/h	σ_y/E	n	σ_E/σ_y	λ_1/λ_c	λ_2/λ_c	β	λ_{max}/λ_c	ξ_{max}
0.5	200	0.0025	10	1.049	2.70	−12.5	1/3	1.0029	0.0043
0.5	200	0.0025	4	1.108	2.73	−11.4	1/3	1.0040	0.0058
0.8	200	0.0025	10	1.040	2.97	−15.2	1/3	1.0023	0.0031
0.8	200	0.0025	4	1.089	2.99	−13.5	1/3	1.0034	0.0045
1.0	200	0.0025	10	1.034	3.23	−22.7	2/5	1.0030	0.0033
1.0	200	0.0025	4	1.078	3.27	−19.4	2/5	1.0047	0.0050